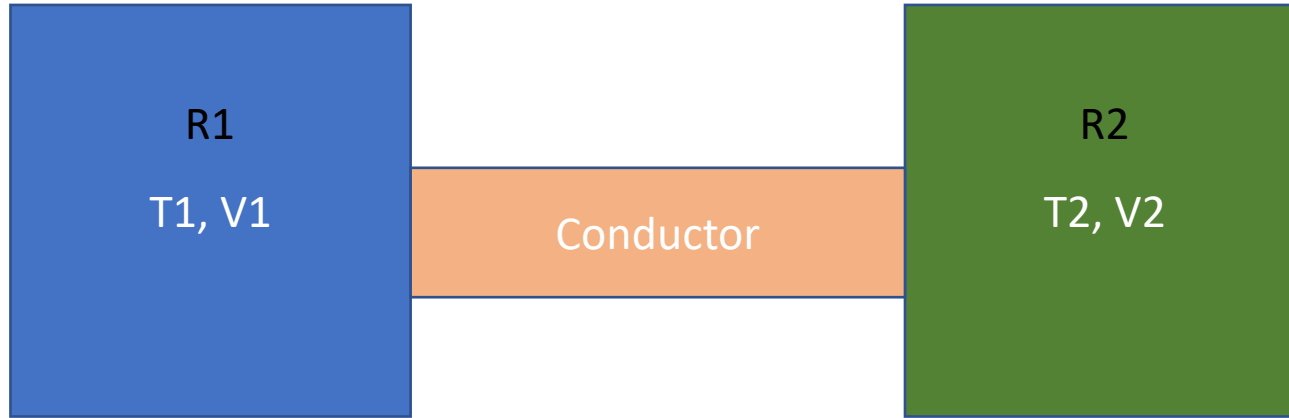


Tutorial #6 :
Irreversible thermodynamics

Exercise #1 : Onsager reciprocity relations



Because of the gradient in temperature and voltage, we can express the flux between the two reservoirs :

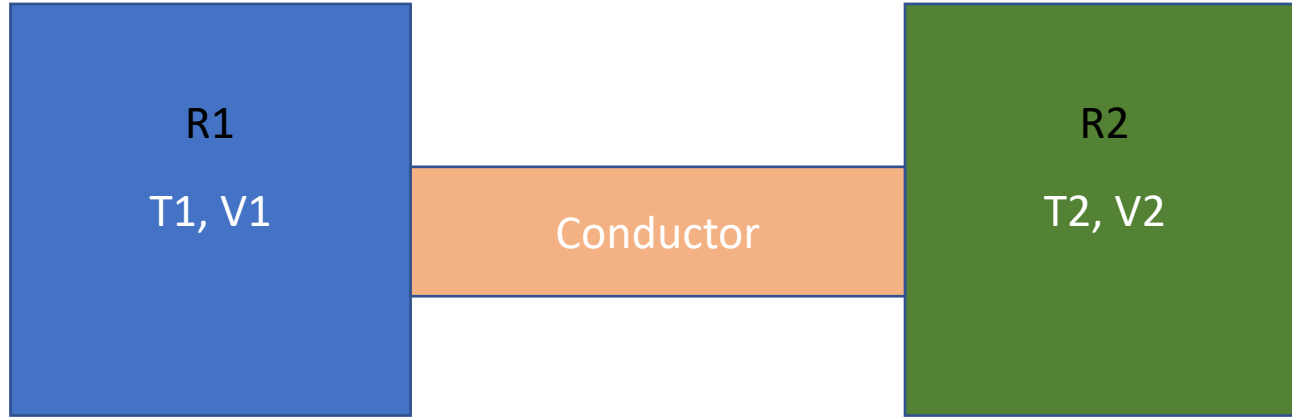
$$\begin{aligned} I_q &= l_{11}\Delta V + l_{12}\Delta T \\ I_U &= l_{21}\Delta V + l_{22}\Delta T \end{aligned}$$

But with this formulation, there is no reciprocity of the coefficients : $l_{21} = l_{12}$ is NOT satisfied

In this exercise, we will define adequate quantities and derive coefficients satisfying reciprocity relations.

Generalized force + exchange of an extensive physical quantity.

Exercise #1 : Onsager reciprocity relations



1) Write an energy and charge budget between the two réservoirs:

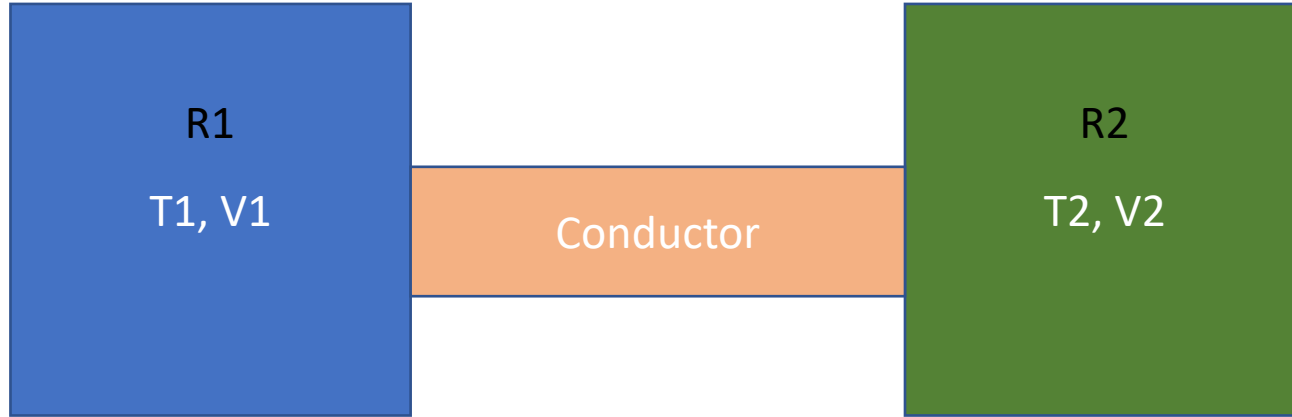
2) Derive the variation of entropy in R1 and R2. You can use the thermodynamic identity :

Because of the gradient in temperature and voltage, we can express the flux between the two reservoirs :

$$\begin{aligned} I_q &= l_{11}\Delta V + l_{12}\Delta T \\ I_U &= l_{21}\Delta V + l_{22}\Delta T \end{aligned}$$

$$dU = TdS + \mu dN + Vdq$$

Exercise #1 : Onsager reciprocity relations



Because of the gradient in temperature and voltage, we can express the flux between the two reservoirs :

$$I_q = l_{11}\Delta V + l_{12}\Delta T$$

$$I_U = l_{21}\Delta V + l_{22}\Delta T$$

1) Write an energy and charge budget between the two réservoirs:

$$q\delta N_1 = -q\delta N_2$$

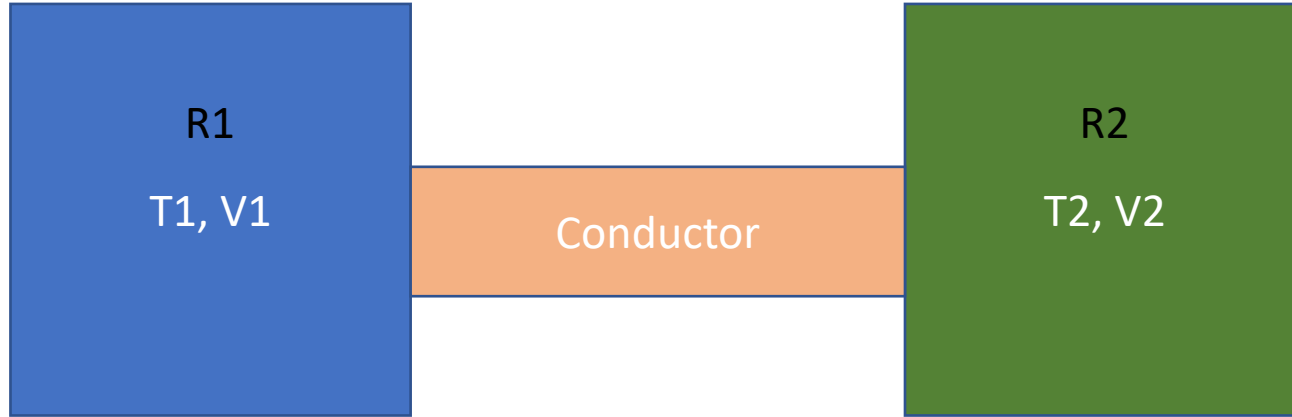
$$\delta U_1 = -\delta U_2$$

2) Derive the variation of entropy in R1 and R2. You can use the thermodynamic identity :

$$\begin{aligned}\delta S_1 &= \frac{\delta U_1}{T_1} - \frac{\mu(T_1) - qV_1}{T_1}\delta N_1 \\ &= -\frac{\delta U_2}{T_1} + \frac{\mu(T_1) - qV_1}{T_1}\delta N_2\end{aligned}$$

$$\delta S_2 = \frac{\delta U_2}{T_2} - \frac{\mu(T_2) + qV_2}{T_2}\delta N_2$$

Exercise #1 : Onsager reciprocity relations

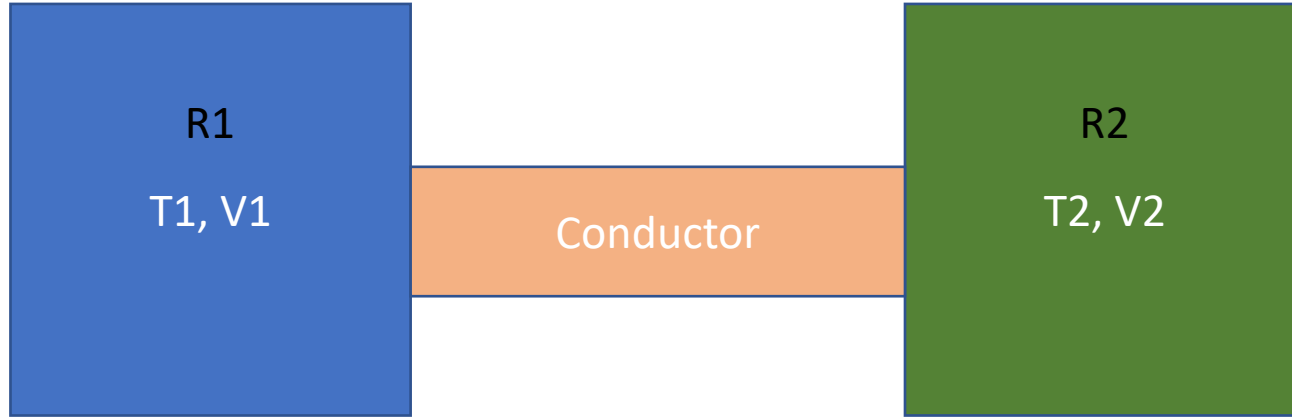


Because of the gradient in temperature and voltage, we can express the flux between the two reservoirs :

$$\begin{aligned} I_q &= l_{11}\Delta V + l_{12}\Delta T \\ I_U &= l_{21}\Delta V + l_{22}\Delta T \end{aligned}$$

3) Derive the total variation of entropy (i.e. variation in both réservoirs)

Exercise #1 : Onsager reciprocity relations



Because of the gradient in temperature and voltage, we can express the flux between the two reservoirs :

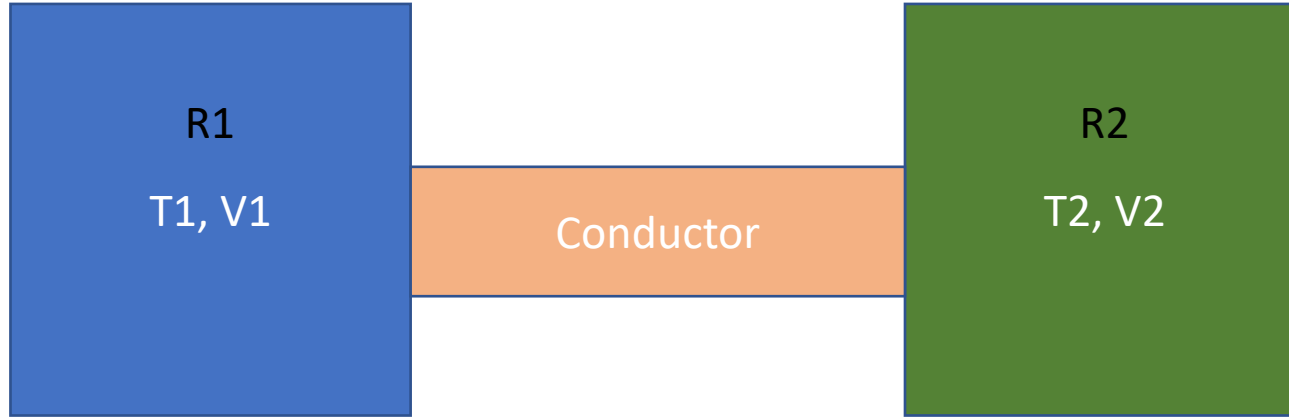
$$I_q = l_{11}\Delta V + l_{12}\Delta T$$

$$I_U = l_{21}\Delta V + l_{22}\Delta T$$

3) Derive the total variation of entropy (i.e. variation in both réservoirs)

$$\begin{aligned}\delta S &= \delta S_1 + \delta S_2 \\ &= \left(\frac{1}{T_2} - \frac{1}{T_1}\right)\delta U_2 + \left(\frac{\mu(T_1) + qV_1}{T_1} - \frac{\mu(T_2) + qV_2}{T_2}\right)\delta N_2\end{aligned}$$

Exercise #1 : Onsager reciprocity relations



Because of the gradient in temperature and voltage, we can express the flux between the two reservoirs :

$$I_q = l_{11}\Delta V + l_{12}\Delta T$$

$$I_U = l_{21}\Delta V + l_{22}\Delta T$$

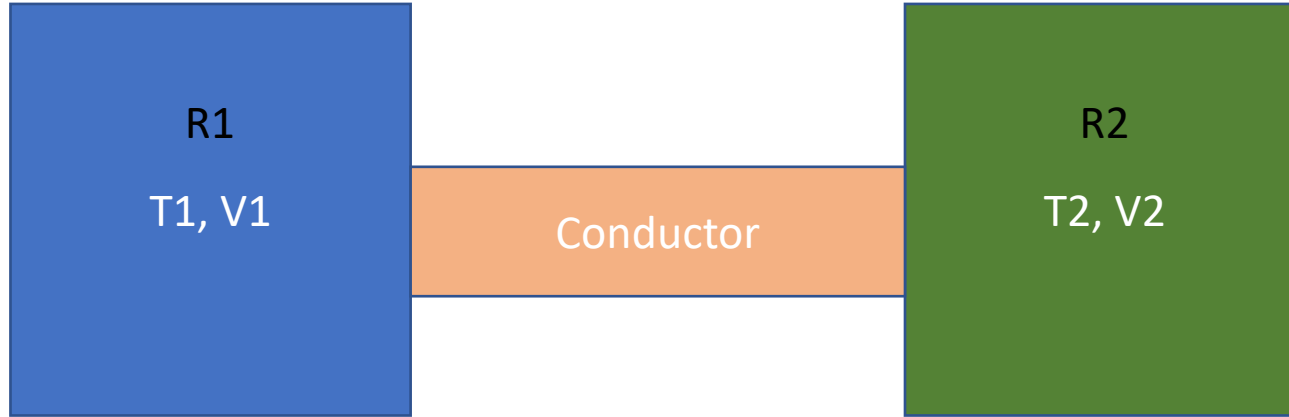
4) Derive the generalized forces X_u and X_q associated to the exchange of energy and charge, knowing that the rate of creation of entropy can be expressed using :

$$\frac{\Delta S}{\Delta t} = \sum_i J_i X_i,$$

With rate of extensive variables given by :

$$J_U = \frac{\Delta U}{\Delta t} \quad J_q = q \frac{\Delta N}{\Delta t}.$$

Exercise #1 : Onsager reciprocity relations



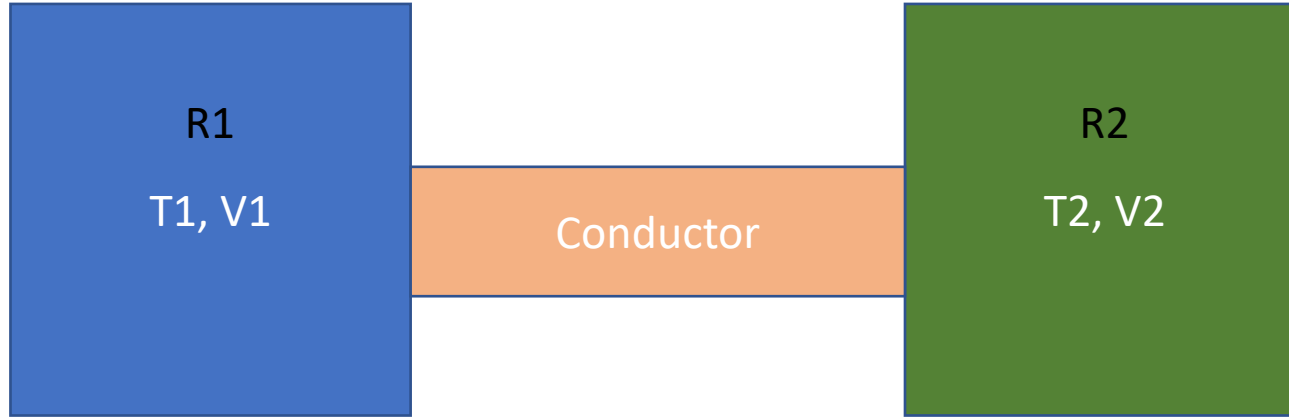
Because of the gradient in temperature and voltage, we can express the flux between the two reservoirs :

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4) Derive the generalized forces X_u and X_q associated to the exchange of energy and charge :

$$\frac{\delta S}{\delta t} = \left(\frac{1}{T_2} - \frac{1}{T_1} \right) \underbrace{\frac{\delta U_2}{\delta t}}_{J_U} + \left(\frac{\mu(T_1)/q + V_1}{T_1} - \frac{\mu(T_2)/q + V_2}{T_2} \right) q \underbrace{\frac{\delta N_2}{\delta t}}_{J_q}$$

Exercise #1 : Onsager reciprocity relations



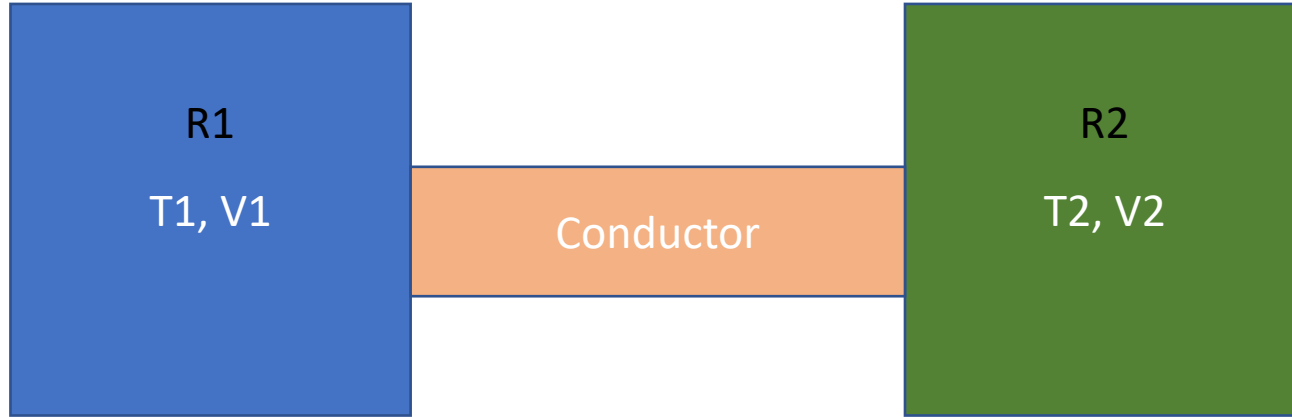
Because of the gradient in temperature and voltage, we can express the flux between the two reservoirs :

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$$\begin{aligned} \frac{\delta S}{\delta t} &= \left(\frac{1}{T_2} - \frac{1}{T_1} \right) \underbrace{\frac{\delta U_2}{\delta t}}_{J_U} + \left(\frac{\mu(T_1)/q + V_1}{T_1} - \frac{\mu(T_2)/q + V_2}{T_2} \right) q \underbrace{\frac{\delta N_2}{\delta t}}_{J_q} \\ &= \Delta\left(\frac{1}{T}\right) J_U - \frac{1}{q} \Delta\left(\frac{\mu + qV}{T}\right) J_q \end{aligned}$$

Exercise #1 : Onsager reciprocity relations



Because of the gradient in temperature and voltage, we can express the flux between the two reservoirs :

$$\begin{aligned} I_q &= l_{11}\Delta V + l_{12}\Delta T \\ I_U &= l_{21}\Delta V + l_{22}\Delta T \end{aligned}$$

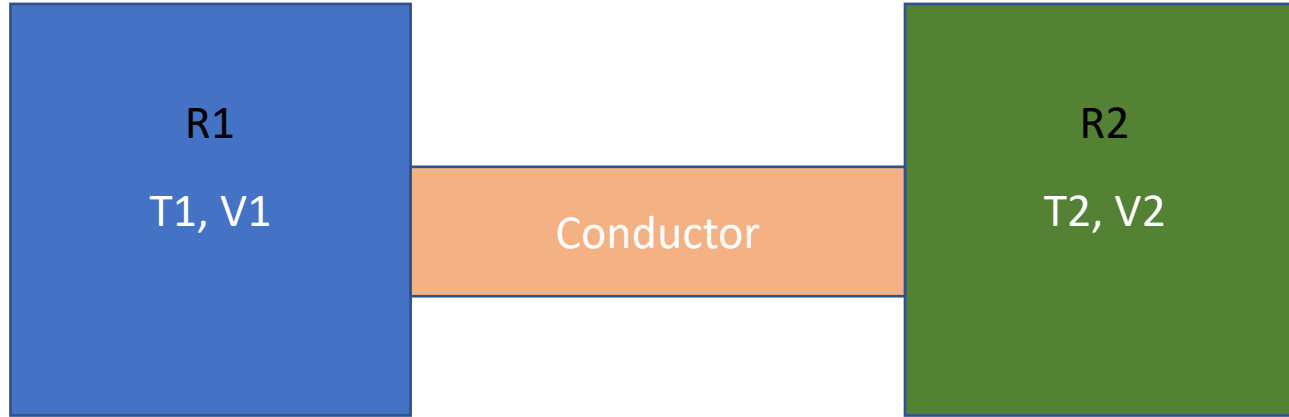
4) Derive the generalized forces X_U and X_q associated to the exchange of energy and charge :

$$\frac{\delta S}{\delta t} = \Delta\left(\frac{1}{T}\right)J_U - \frac{1}{q}\Delta\left(\frac{\mu + qV}{T}\right)J_q$$

$$X_U = \Delta\left(\frac{1}{T}\right) = -\frac{\Delta T}{T^2}$$

$$X_q = -\frac{1}{q}\Delta\left(\frac{\mu_{ec}}{T}\right)$$

Exercise #1 : Onsager reciprocity relations



Because of the gradient in temperature and voltage, we can express the flux between the two reservoirs :

$$I_q = l_{11}\Delta V + l_{12}\Delta T$$

$$I_U = l_{21}\Delta V + l_{22}\Delta T$$

$$J_q = L_{11}X_q + L_{12}X_U$$

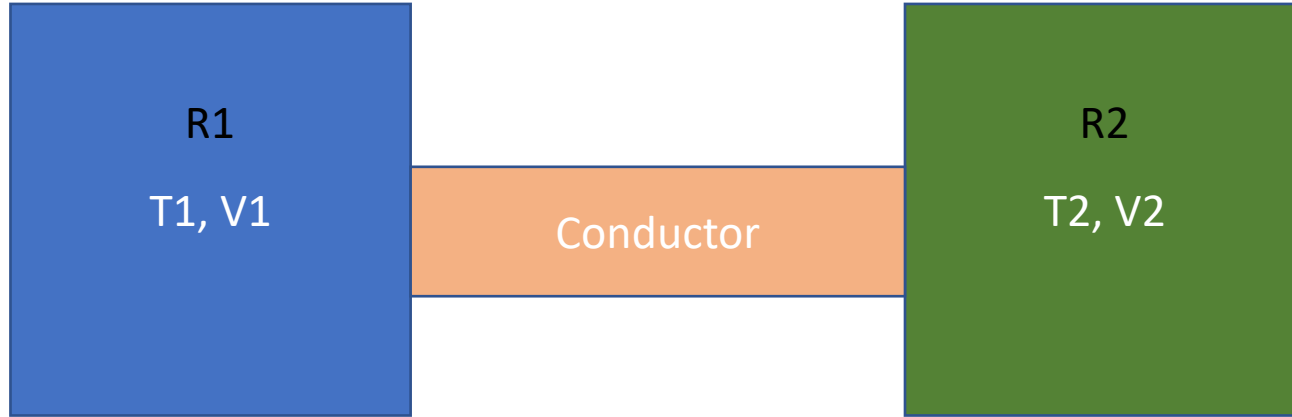
$$J_U = L_{21}X_q + L_{22}X_U$$

We know now how to define coefficients that satisfy Onsager reciprocity

5) Derive the thermal conductance given by $J_U = -\Gamma\Delta T$

Which is given in absence of charge flux (instead of zero voltage) !

Exercise #1 : Onsager reciprocity relations



Because of the gradient in temperature and voltage, we can express the flux between the two reservoirs :

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$$I_U = l_{21}\Delta V + l_{22}\Delta T$$

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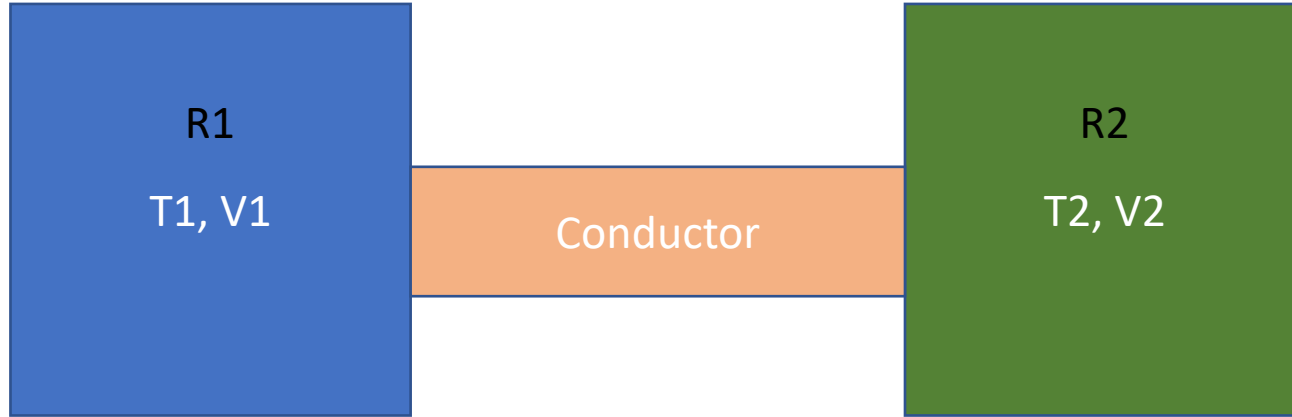
$$J_U = L_{21}X_q + L_{22}X_U$$

We know now how to define coefficients that satisfy Onsager reciprocity

$$J_U = -\Gamma\Delta T$$

$$= L_{21}X_q + L_{22}X_U$$

Exercise #1 : Onsager reciprocity relations



Because of the gradient in temperature and voltage, we can express the flux between the two reservoirs :

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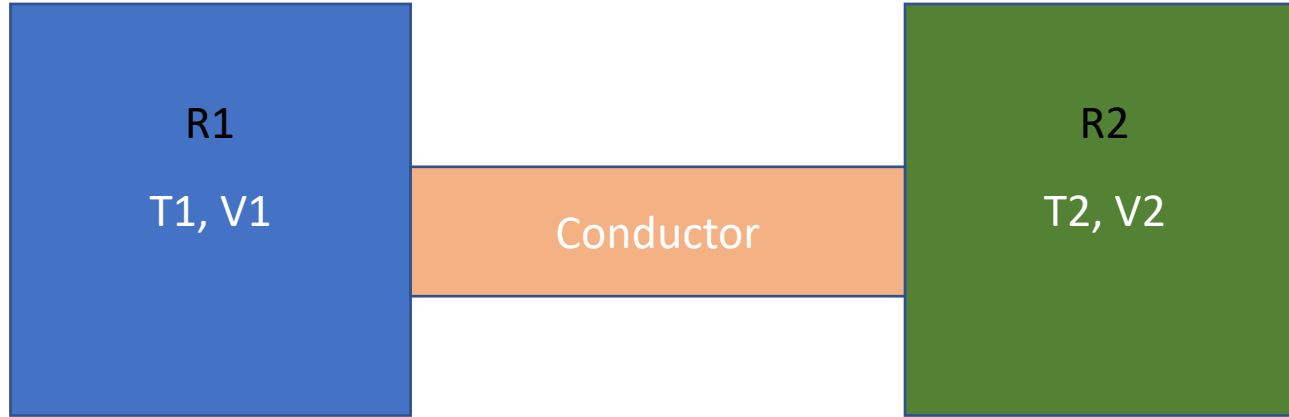
$$J_U = -\Gamma\Delta T$$

$$= L_{21}X_q + L_{22}X_U$$

$$J_q = 0$$

$$X_q = -\frac{L_{12}}{L_{11}}X_U \quad \text{with} \quad X_U = \Delta\left(\frac{1}{T}\right) = -\frac{\Delta T}{T^2}$$

Exercise #1 : Onsager reciprocity relations



Because of the gradient in temperature and voltage, we can express the flux between the two reservoirs :

$$I_q = l_{11}\Delta V + l_{12}\Delta T$$

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We know now how to define coefficients that satisfy Onsager reciprocity

$$J_U = -\Gamma\Delta T$$

$$= L_{21}X_q + L_{22}X_U$$

$$J_q = 0$$

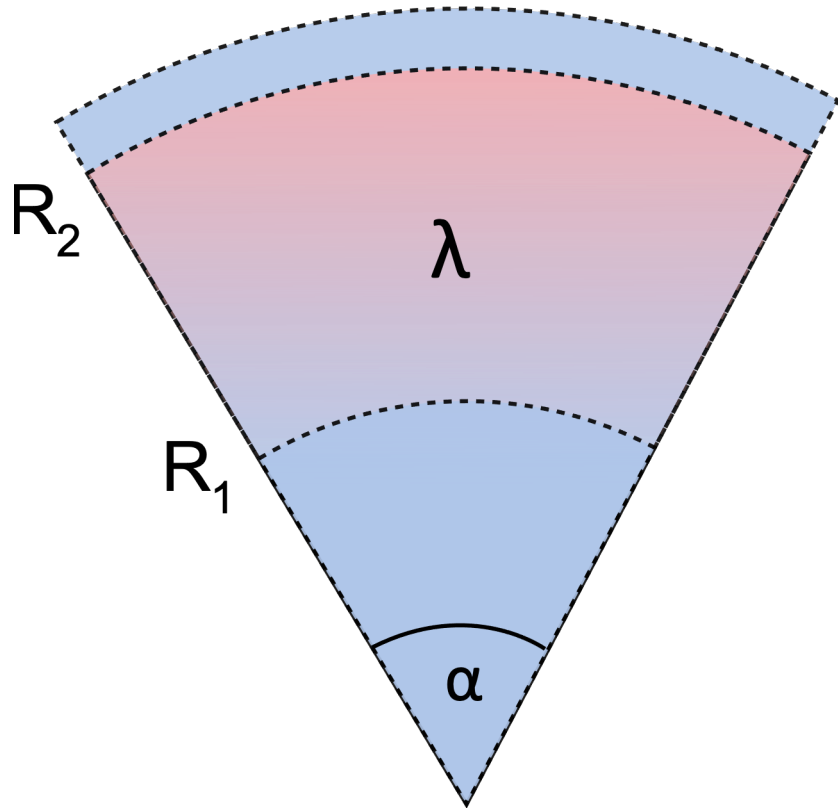
$$X_q = -\frac{L_{12}}{L_{11}}X_U \quad \text{with} \quad X_U = \Delta\left(\frac{1}{T}\right) = -\frac{\Delta T}{T^2}$$

$$-\Gamma\Delta T = -\frac{L_{21}L_{12}}{L_{11}}X_U + L_{22}X_U$$

$$\Gamma = \frac{L_{21}L_{12} - L_{22}L_{11}}{L_{11}} \frac{-1}{T^2}$$

$$= \frac{L_{22}L_{11} - L_{12}^2}{L_{11}T^2}$$

Exercise #2 : Heat exchange in a constriction



$$\mathbf{J}_U = -\lambda \vec{\nabla} T = -\lambda \frac{\partial T}{\partial r} \mathbf{u}_r$$

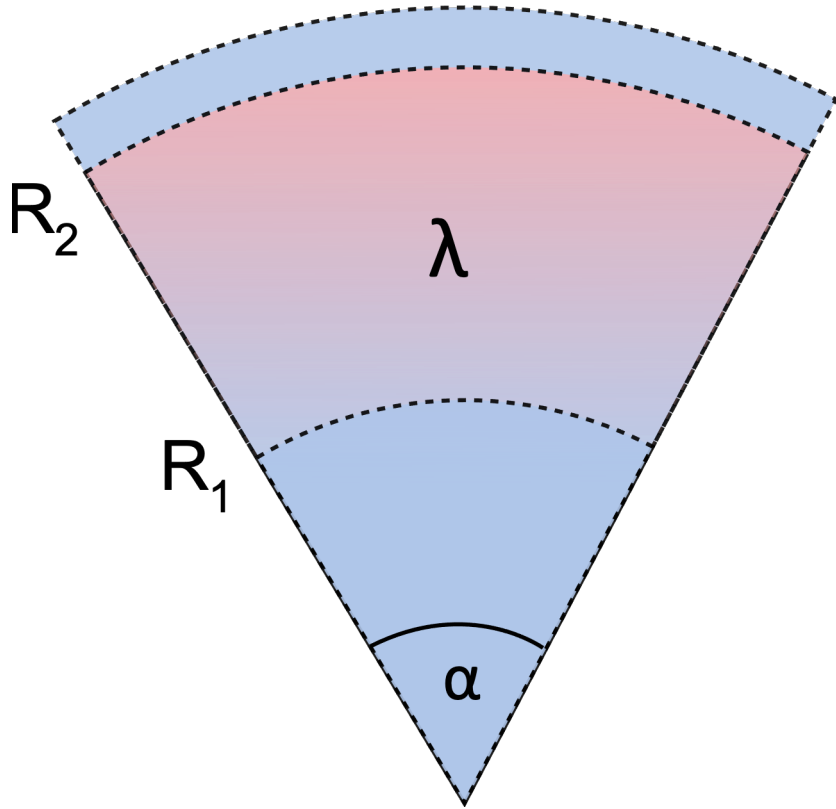
Radial flux of heat across
« shell portions » defined by $\Sigma(r)$

$$\Omega = 2\pi(1 - \cos \alpha)$$

$$\Sigma(r) = \Omega r^2 = 2\pi(1 - \cos \alpha) r^2$$

- 1) Rate of local volumic entropy creation ? (remember it is affinity x flux)
- 2) Show that it is proportionnal to $1/r^4$ (use the fact that the flux is constant across $\Sigma(r)$)
- 3) Where do irreversible phenomena occur most in the system ?

Exercise #2 : Heat exchange in a constriction



$$\mathbf{J}_U = -\lambda \vec{\nabla} T = -\lambda \frac{\partial T}{\partial r} \mathbf{u}_r$$

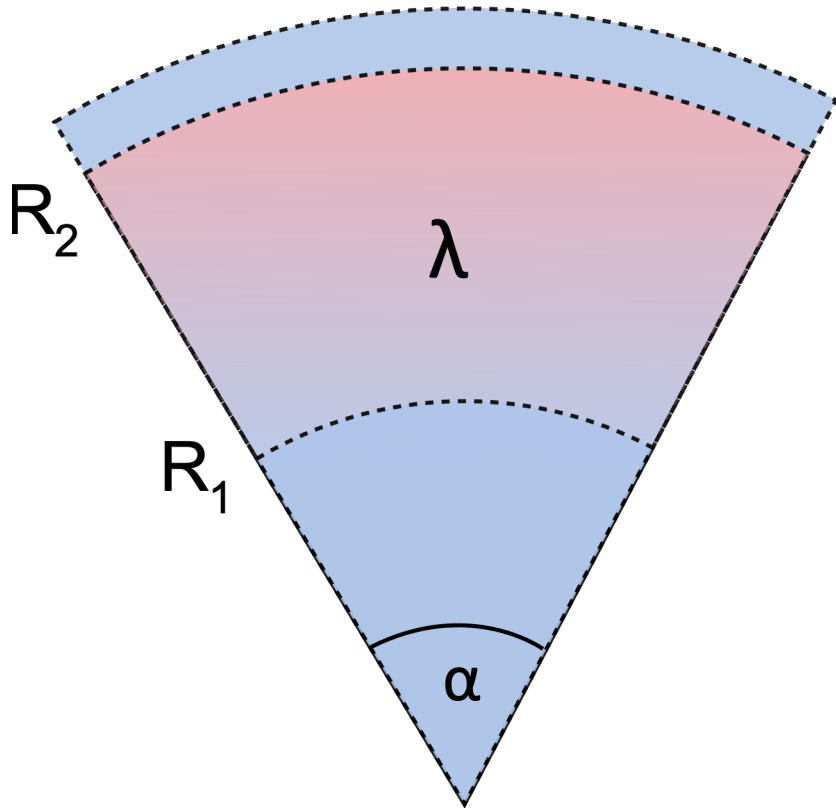
$$\Omega = 2\pi(1 - \cos \alpha)$$

$$\Sigma(r) = \Omega r^2 = 2\pi(1 - \cos \alpha) r^2$$

- 1) Rate of local volumic entropy creation ? (remember it is affinity x flux)

$$\begin{aligned} \frac{\partial s}{\partial t} &= \vec{\nabla} \left(\frac{1}{T} \right) \cdot \mathbf{J}_U \\ &= \frac{\lambda}{T^2} \vec{\nabla} T \cdot \vec{\nabla} T \\ &= \frac{\lambda}{T^2} \left(\frac{\partial T}{\partial r} \right)^2 \end{aligned}$$

Exercise #2 : Heat exchange in a constriction



$$\mathbf{J}_U = -\lambda \vec{\nabla} T = -\lambda \frac{\partial T}{\partial r} \mathbf{u}_r$$

$$\Omega = 2\pi(1 - \cos \alpha)$$

$$\Sigma(r) = \Omega r^2 = 2\pi(1 - \cos \alpha)r^2$$

2) Show that it is proportionnal to $1/r^4$ (use the fact that the flux is constant across $\Sigma(r)$)

$$\mathbf{J}_u(r) \cdot \Sigma(r) = \text{cste}$$

$$-\lambda \frac{\partial T}{\partial r} 2\pi(1 - \cos \alpha)r^2 = \text{cste}$$

$$\frac{\partial T}{\partial r} = \frac{A}{r^2}$$

$$\frac{\partial s}{\partial t} = \frac{\lambda}{T^2} \left(\frac{A}{r^2} \right)^2 \approx \frac{1}{r^4}$$